

Interpolation method for quaternionic-Bézier curves

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Abstract. We study rational quaternionic-Bézier curves in three dimensional space. We construct the quadratic quaternionic-Bézier curve which interpolates five points, or three points and two tangent vectors.

Keywords: Quaternionic-Bézier curve, interpolation.

Introduction

We analyse rational Bézier curves with quaternion control points and weights, called quaternionic-Bézier (QB) curves. This class of curves has two remarkable properties:

- a QB-curve of degree n can be converted to the classical rational Bézier curve of degree $2n$;
- QB-curves are invariant with respect to Möbius transformations.

The QB-curves of degree one are circles. They were discussed in [6]. Quadratic QB-curves were described in [7, 3]. However, this description is not convenient, because the middle control may be in 4-dimensional space and is not clear how to use this point in practise for modelling purposes. In this paper we give two interpolation constructions for quadratic QB-curves:

- the interpolation curve through five points in \mathbb{R}^3 ,
- the interpolation curve through three points with prescribed tangent vectors at the endpoints.

We use the idea of Anton Gfrerrer [1] to construct a curve for the interpolation method on the hyperquadric. In order to use this we notice the one-to-one correspondence between quaternionic curves and the curves on Study quadric in \mathbb{R}^8 (see also [4]). On the another hand, points on the Study quadric can be represented as the displacements in \mathbb{R}^3 , while curves on the Study quadrics mean the motion in \mathbb{R}^3 . Therefore, QB-curves could be important in kinematics applications (see [2, 4]).

1 Notations and definitions

Let us denote by \mathbb{R} , \mathbb{C} , \mathbb{H} the set of real numbers, complex numbers and quaternion numbers respectively. The quaternions \mathbb{H} can be identified with \mathbb{R}^4

$$\mathbb{H} = \{q = [r, p] \mid r \in \mathbb{R}, p \in \mathbb{R}^3\} = \mathbb{R}^4,$$

where $r = \text{Re}(q)$, $p = \text{Im}(q)$ denote real and imaginary parts of a quaternion $q = [r, p]$. The multiplication in the algebra \mathbb{H} is defined by the formula

$$[r_1, p_1][r_2, p_2] = [r_1 r_2 - p_1 \cdot p_2, r_1 p_2 + r_2 p_1 + p_1 \times p_2],$$

where $p_1 \cdot p_2$, $p_1 \times p_2$ are scalar and vector products in \mathbb{R}^3 . Let $\bar{q} = [r, -p]$ means the conjugate quaternion, and $|q| = \sqrt{r^2 + p \cdot p} = \sqrt{q\bar{q}}$ denotes the length of the quaternion. The multiplicative inverse of q is $q^{-1} = \bar{q}/|q|^2 = [r/|q|^2, -p/|q|^2]$, i.e. $qq^{-1} = q^{-1}q = 1$. We identify the set of pure imaginary quaternions with \mathbb{R}^3 : $\text{Im}(\mathbb{H}) = \{[0, p] \mid p \in \mathbb{R}^3\} = \mathbb{R}^3$.

2 The Study quadric and QB-curves

We consider a pair of quaternions $(p; q) \in \mathbb{H} \times \mathbb{H} = \mathbb{R}^8$ as a point in the projective space \mathbb{P}^7 . The *Study quadric* SQ is a hypersurface in \mathbb{P}^7 defined by the equation $p\bar{q} + q\bar{p} = 0$. Explicitly, let $p = [p_1, \dots, p_4]$, $q = [q_1, \dots, q_4]$ be two quaternions then the equation of the Study quadric is $\sum_1^4 p_i q_i = 0$:

$$SQ := \{(p; q) = (p_1, p_2, p_3, p_4; q_1, q_2, q_3, q_4) \mid p_1 q_1 + p_2 q_2 + p_3 q_3 + p_4 q_4 = 0\}.$$

Geometrically, $(p; q) \in SQ$ if and only if the vector p is orthogonal to the vector q in the Euclidean sense. The point on the Study quadric $c = (p; q) \in SQ$ defines a point in \mathbb{R}^3 :

$$\Pi : (p; q) \rightarrow qp^{-1} \in \text{Im}(\mathbb{H}) = \mathbb{R}^3,$$

because $\text{Re}(qp^{-1}) = \text{Re}(q\bar{p}/p\bar{p}) = \sum_1^4 q_i p_i / p\bar{p} = 0$.

An important application of the Study quadric is modelling of rigid body displacements. A dual quaternion $c = (p; q) \in SQ$ acts on the quaternion $x = [0, x_1, x_2, x_3]$ by the formula

$$c : x \rightarrow \frac{px\bar{p} + p\bar{q} - q\bar{p}}{p\bar{p}} = \frac{px\bar{p} - 2q\bar{p}}{p\bar{p}} = (px - 2q)p^{-1}.$$

The first part of the above formula pxp^{-1} means rotation while the second means translation, therefore this action is an element of $SE(3)$, the group of rigid body displacement (see for details [2]).

The rational quaternionic curve $c(t)$ can be defined as:

$$c(t) = q(t)p(t)^{-1}, \quad \text{where } q(t), p(t) \in \mathbb{H}[t] \text{ are quaternion polynomials.}$$

For applications it is important to describe curves in three dimensional space. We observe that

$$c(t) = q(t)p(t)^{-1} \in \text{Im}(\mathbb{H}) = \mathbb{R}^3 \quad \text{if and only if } (p(t); q(t)) \in SQ, \text{ i.e.}$$

a rational QB-curve in 3D is the same as a curve on the Study quadric.

3 Interpolation construction for QB-curves

Rational quadratic quaternionic-Bézier curves were considered in [7]. Our interpolation construction of the QB-curve was inspired by the idea A. Gferrer (see [1]) of interpolation points on the Study quadric. The arbitrary point $c = (p; q) \in SQ$ can be presented in the homogeneous form

$$c = (p; q) = (pq^{-1}q; q) = (a_0w_0; w_0), \text{ where } a_0 = pq^{-1} \in \text{Im}(\mathbb{H}) = \mathbb{R}^3, w_0 = q,$$

which we interpret as the point a_0 in \mathbb{R}^3 with a quaternion weight w_0 .

Let $n \geq 1$ be an integer, and let $T = [t_0, \dots, t_n]$ be $n + 1$ pairwise different real parameter values. Then we define polynomials of degree n

$$f_i(t) = \prod_{k \neq i} (t - t_k), \quad \text{with the following properties}$$

$$f_i(t_i) \neq 0, \quad f_i(t_j) = 0, \quad \text{if } j \neq i.$$

Let us fix $n + 1$ homogeneous points $(a_{2i}w_{2i}; w_{2i}), i = 0, \dots, n$ and define quaternionic polynomials

$$q(t) = \sum_{i=0}^n a_{2i} w_{2i} f_i(t), \quad p(t) = \sum_{i=0}^n w_{2i} f_i(t), \quad C(t) = q(t) p(t)^{-1}. \quad (1)$$

We are going to find conditions when the curve $C(t) = q(t)p(t)^{-1}$ is in $\text{Im}(\mathbb{H})$. First of all we note, that

$$C(t_i) = a_{2i} \in \text{Im}(\mathbb{H}) = \mathbb{R}^3, \quad i = 0, 1, \dots, n,$$

for arbitrary weights $w_i, i = 0, 1, \dots, n$ (because $f_j(t_i) = 0, j \neq i$). Let $S = [s_1, \dots, s_n]$ be different (from the set T) real parameters (i.e. $S \cap T = \emptyset$) and $a_{2j-1} \in \text{Im}(\mathbb{H}), j = 1, \dots, n$ be some points in \mathbb{R}^3 . We consider the linear system

$$C(s_j) = a_{2j-1}, \quad j = 1, \dots, n.$$

This linear system is equivalent to $q(s_j) = a_{2j-1} p(s_j), j = 1, \dots, n$, i.e.

$$\sum_{i=0}^n a_{2i} w_{2i} f_i(s_j) = \sum_{i=0}^n a_{2j-1} w_{2i} f_i(s_j), \quad j = 1, \dots, n, \text{ or explicitly,}$$

$$\sum_{i=1}^n (a_{2i} - a_{2j-1}) f_i(s_j) w_{2i} = (a_{2j-1} - a_0) f_0(s_j) w_0, \quad j = 1, \dots, n. \quad (2)$$

The quaternion linear system (2) with n equations and n unknowns w_2, w_4, \dots, w_{2n} has a unique solution if the corresponding matrix $A = (\alpha_{ij})$ is not singular.

Theorem 1. *Assume the matrix $\alpha_{ij} = (a_{2i} - a_{2j-1}) f_i(s_j), i, j = 1, \dots, n$, is non-singular (or invertible). Then there are unique (up to left multiplication) weights $w_{2i}, i = 0, \dots, n$, such that the rational curve $C(t)$ defined by the formula (1) is in $\text{Im}(\mathbb{H}) = \mathbb{R}^3$. Moreover, the curve $C(t)$ interpolates points $a_i, i = 0, \dots, 2n$; actually $C(t_i) = a_{2i}, i = 0, \dots, n$, and $C(s_i) = a_{2i-1}, i = 1, \dots, n$.*

Proof. The non-singular quaternion matrix A has an LU-decomposition [5, Theorem 3.1]. There exists a decomposition $PA = LU$ and the matrix A is invertible $A^{-1} = U^{-1}L^{-1}P$. Therefore, the system (2) has a unique solution for the weights w_2, w_4, \dots, w_{2n} . We can take $w_0 = 1$ and construct the curve $C(t)$. This curve is in \mathbb{R}^3 for the set $T \cup S$ of cardinality $2n + 1$. Hence, according to Lemma 1 below, the curve $C(t)$ is in \mathbb{R}^3 . \square

Lemma 1. *The rational curve $C(t) = q(t)p(t)^{-1}$ is an imaginary quaternion for all parameters t if and only if $\operatorname{Re}(C(\beta_i)) = 0$ for some real different parameters β_i , $i = 0, 1, \dots, 2n$.*

Proof. We present the rational curve $C(t)$ as follows:

$$C(t) = q(t)p(t)^{-1} = \frac{q(t)\bar{p}(t)}{p(t)\bar{p}(t)}.$$

The numerator $q(t)\bar{p}(t)$ is the quaternion polynomial of degree $2n$. If $\operatorname{Re}(C(\beta_i)) = 0$ for some real different parameters β_i , $i = 0, 1, \dots, 2n$, then the real polynomial $\operatorname{Re}(q(t)\bar{p}(t))$ of degree $2n$ is zero on $2n + 1$ different parameter values, i.e. $\operatorname{Re}(q(t)\bar{p}(t)) = 0$. \square

Let us fix

$$T = [0, 1/2, 1], \quad S = [1/4, 3/4], \quad (3)$$

and discuss the case $n = 2$ in greater detail. We choose five different points $a_0, a_1, \dots, a_4 \in \mathbb{R}^3$. Then the linear system (2) multiplied by 16 is

$$e_1 : -3d_{21}w_2 - d_{41}w_4 = 3d_{10}w_0, \quad (4)$$

$$e_2 : -3d_{23}w_2 + 3d_{43}w_4 = -d_{30}w_0, \quad \text{where } d_{ij} = a_i - a_j. \quad (5)$$

In order to solve it, we eliminate w_2 in the equation $3d_{41}^{-1}e_1 + d_{43}^{-1}e_2$, and w_4 in the equation $d_{21}^{-1}e_1 - d_{23}^{-1}e_2$. Finally, we get

$$w_2 = (-9d_{41}^{-1}d_{21} - 3d_{43}^{-1}d_{23})^{-1}(9d_{41}^{-1}d_{10} - d_{43}^{-1}d_{30})w_0, \quad (6)$$

$$w_4 = (-d_{21}^{-1}d_{41} - 3d_{23}^{-1}d_{43})^{-1}(3d_{21}^{-1}d_{10} + d_{23}^{-1}d_{30})w_0. \quad (7)$$

The above formulas for weights are correct if $(-9d_{41}^{-1}d_{21} - 3d_{43}^{-1}d_{23}) \neq 0$ and $(-d_{21}^{-1}d_{41} - 3d_{23}^{-1}d_{43}) \neq 0$. Both inequalities are equivalent to the inequality

$$d_{43}^{-1}d_{32}d_{21}^{-1}d_{14} \neq -3. \quad (8)$$

The expression $d_{43}^{-1}d_{32}d_{21}^{-1}d_{14}$ is the cross-ratio of four points a_4, a_3, a_2, a_1 , which is a real number if and only if these four points are on a circle (see for example [8]). Geometrically, the inequality (8) means that four points are not circular or they are circular but the cross-ratio is not equal to -3 .

Corollary 1. *The interpolation curve $C(t)$ ($n = 2$) defined by (1) with five points $C(i/4) = a_i$, $\in \mathbb{R}^3$, $i = 0, 1, \dots, 4$, and the weights w_2, w_4 as in formulas (6), (7) is in $\operatorname{Im}(\mathbb{H}) = \mathbb{R}^3$. The formulas for weights are well defined if the inequality (8) holds, i.e. points a_4, \dots, a_1 are not on a circle or they are circular but the cross-ratio is not equal to -3 .*

For applications it is also important to know tangent vectors. Let $C'(t_0)$ be the tangent vector at the starting point a_0 and $C'(t_n)$ – the tangent vector at the end point a_4 of the curve. If we replace two conditions $C(s_i) = a_{2i-1}$, $i = 1, 2$, with the conditions $C'(t_0) = v_0 \in \text{Im}(\mathbb{H})$, $C'(t_n) = v_1 \in \text{Im}(\mathbb{H})$ we obtain the linear system

$$\begin{aligned} f'_1(t_0) d_{20} w_2 + f'_2(t_0) d_{40} w_4 &= f_0(t_0) v_0 w_0, \\ f'_1(t_n) d_{24} w_2 - f'_2(t_n) v_1 w_4 &= f'_0(t_n) d_{40} w_0. \end{aligned}$$

Eliminating w_2, w_4 we get the following solution

$$w_2 = (-2 d_{40}^{-1} d_{20} - 2 v_1^{-1} d_{24})^{-1} (d_{40}^{-1} v_0 - v_1^{-1} d_{40}) w_0, \tag{9}$$

$$w_4 = (-2 d_{20}^{-1} d_{40} - 2 d_{24}^{-1} v_1)^{-1} (2 d_{20}^{-1} v_0 + 2 d_{24}^{-1} d_{40}) w_0. \tag{10}$$

The above formulas for weights are well defined if

$$v_1 \neq -d_{42} d_{20}^{-1} d_{04}. \tag{11}$$

According to Remark 4.5 in [8] $d_{42} d_{20}^{-1} d_{04}$ is the tangent vector to the circle c_{420} through a_4, a_2, a_0 at the point a_4 . Therefore, the condition (11) means that the vector v_1 is not tangent vector to the circle through the point a_4 .

Corollary 2. *In the case $n = 2$ the interpolation curve $C(t)$ defined by (1) with three points $C(0) = a_0$, $C(1/2) = a_2$, $C(1) = a_4$ in \mathbb{R}^3 and the weights w_2, w_4 defined in formulas (9), (10) is in $\text{Im}(\mathbb{H}) = \mathbb{R}^3$. Moreover, the curve $C(t)$ has the tangent vectors $C'(0) = v_0$ and $C'(1) = v_1$ in \mathbb{R}^3 at the points a_0 and a_4 , respectively. The formulas for weights are well defined if the inequality (11) holds. In particular, if the vector v_1 is not a tangent vector to the circle through a_4, a_2, a_0 at the point a_4 then the weights are well defined by (9) and (10).*

We can write the curve $C(t)$ in Bézier form. For this we express

$$f_0 = \frac{1}{2}\beta_0 - \frac{1}{4}\beta_1, \quad f_1 = -\frac{1}{2}\beta_1, \quad f_2 = -\frac{1}{4}\beta_1 + \frac{1}{2}\beta_2,$$

where quadratic Bernstein polynomials are $\beta_i = \beta_i^2(t) = \binom{2}{i}(1-t)^{2-i}t^i$. Let

$$\begin{aligned} u_0 &= w_0, & u_1 &= (-1/2)(w_0 + 2w_2 + w_4), & u_2 &= w_4, \\ p_0 &= a_0, & p_1 &= (-1/2)(a_0w_0 + 2a_2w_2 + a_4w_4)(u_1)^{-1}, & p_2 &= a_4. \end{aligned}$$

Then the curve $C(t)$ can be presented in the Bézier form with new homogeneous points $(p_i u_i, u_i)$

$$C(t) = \left(\sum_{i=0}^2 p_i u_i \beta_i \right) \left(\sum_{i=0}^2 u_i \beta_i \right)^{-1}.$$

We note that the middle control point p_1 usually is not in 3D (see [7]).

Remark 1. If we change the parameter values T, S defined by formulas (3) the interpolation curve $C(t)$ would be different. In fact then formulas for weights (6), (7), (9), (10) must be recalculated too.

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REZIUMĖ

Interpoliacijos metodas kvaternioninėms Bézier kreivėms

S. Zubė

Darbe yra aprašytas racionalios kvaternioninės Bézier kreivės interpoliacinis uždavinys. Pagrindinis dėmesys yra sutelktas į kvaternionines konikes. Gautos sąlygos, kada jos guli trimatėje erdvėje, kas yra svarbu taikymuose.

Raktiniai žodžiai: kvaternioninės kreivės, interpoliacijos.